

Calculation of formant frequencies  
of twin-tube and n-tube approximations  
of the vocal tract.

- J.G.Blom, E.O.Kappner -

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## 1. Summary

In this report two programs in Basic Fortran IV are described, which calculate the formant frequencies of models of the vocal tract. The first program calculates the formant frequencies of the so-called twin-tube model. The second, which can be considered as a further development of the twin-tube program, takes a series of 20 connected tubes, each with uniform cross-area, as an approximation of the vocal tract. In both programs the calculations are based on the theory of four terminal networks and the bi-section iteration method of Bolzano. The programs are primarily written for an IBM 1130 system, but can easily be modified for other systems. The console typewriter is used for the input of the parameters. The programs are self-instructing.

## 2. Introduction

The literature on the calculation of formant frequencies mentions several models of the vocal tract. They all are one-dimensional models. In most cases the boundary conditions are:  $u = 0$  ( $u =$  velocity) at the vocal cords, and  $p = 0$  ( $p =$  sound pressure) at the lips. Two types of models can be distinguished:

- (a) models in which the cross area is a continuous function of place,
- (b) models in which the vocal tract is approximated by a number of tubes with uniform cross-areas.

Examples of type (a) are presented in calculations based on Webster's horn equation, as done, for example, by Ungeheuer (1). A well-known model of type (b) is the so-called twin-tube, which was presented first by Dunn (2), and later by Fant (3). Mol's formula (4), which is built on other parameters, is easier to handle. Since the twin-tube equation is transcendental, in the general case its solution can only be found by numerical methods.

In the case of vocal tract models consisting of a greater number of tubes, it is hardly possible to derive manageable equations. Using a computer, it is possible to avoid the derivation of the equation, as will be shown later on (4.2.6.).

In this report two programs are presented. Both are written in Basic Fortran IV for an IBM 1130 system, but can easily be modified for other systems. The first program, written by Blom, is a numerical solution of the twin-tube equation. The second, the  $n$ -tube program,

written by Blom and Kappner, uses an algorithm to determine the formant frequencies of a chain of an arbitrary number of tubes. For practical reasons the number of tubes is limited to 20 in this program. In modifications for other computing systems this limit can be adapted to the precision of the system. Further work in this field is in progress, and will be reported upon later.

In this report the following notations are used:

- S is the cross-area of the tube,
- u is the velocity of the air particles,
- v is the volume velocity (  $v = S.u$  ) ,
- c is the velocity of sound propagation,
- p is the sound pressure,
- $\rho$  is the density,
- f is the frequency,
- $\omega$  is the angular frequency (  $\omega = 2\pi f$  ) .

### 3. Basic Principles

#### 3.1. Four-pole theory.

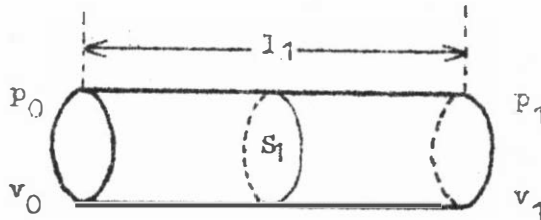


Fig.1

For a tube with uniform cross area, which has a length  $l_1$  and a cross area  $S_1$ , the relation between pressure and volume velocity at both ends ( $p_0, v_0$  and  $p_1, v_1$  respectively) is given by:

$$\begin{bmatrix} p_0 \\ v_0 \end{bmatrix} = \begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix} \begin{bmatrix} p_1 \\ v_1 \end{bmatrix}$$

where  $A_1$ ,  $B_1$ ,  $C_1$  and  $D_1$  are the four-pole coefficients:

$$A_1 = \cos \frac{\omega l_1}{c}, \quad B_1 = i \frac{\rho c}{S_1} \sin \frac{\omega l_1}{c},$$

$$C_1 = i \frac{S_1}{\rho c} \sin \frac{\omega l_1}{c}, \quad D_1 = \cos \frac{\omega l_1}{c}.$$

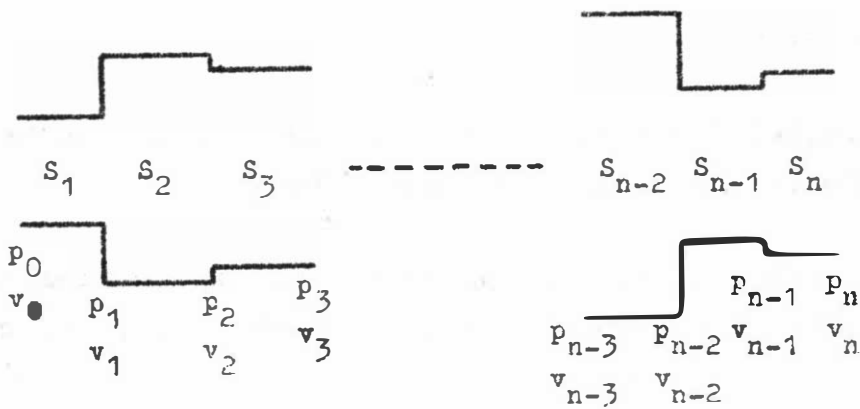


Fig. 2

For \$n\$ connected tubes with uniform cross areas, with lengths and cross areas respectively \$l\_1, l\_2, l\_3, \dots, l\_n\$ and \$S\_1, S\_2, S\_3, \dots, S\_n\$, and pressure and volume velocity at the end of each as given in fig. 2, we have:

$$\begin{bmatrix} p_0 \\ v_0 \end{bmatrix} = \begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix} \begin{bmatrix} A_2 & B_2 \\ C_2 & D_2 \end{bmatrix} \dots \dots \begin{bmatrix} A_{n-1} & B_{n-1} \\ C_{n-1} & D_{n-1} \end{bmatrix} \begin{bmatrix} A_n & B_n \\ C_n & D_n \end{bmatrix} \begin{bmatrix} p_n \\ v_n \end{bmatrix}$$

If we define:

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \prod_{i=1}^n \begin{bmatrix} A_i & B_i \\ C_i & D_i \end{bmatrix},$$

then we have

$$\begin{bmatrix} p_0 \\ v_0 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} p_n \\ v_n \end{bmatrix}.$$

Assuming that the closed ending (vocal cords) is at the first tube,

and the open ending (lips) at the n'th, we have as boundary conditions:

$$v_0 = 0 \quad \text{and} \quad p_n = 0 \quad .$$

Thus:

$$\begin{bmatrix} p_0 \\ 0 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} 0 \\ v_0 \end{bmatrix} \quad .$$

Then the condition :

$$D = 0 \quad (1)$$

must be fulfilled. This is an equation in  $\omega$  ; the solutions give us the resonance frequencies of the system.

For a small number of tubes, the matrix multiplication can easily be carried out. In the case  $n = 2$  ( twin-tube ) , the condition (1) becomes:

$$C_1 B_2 + D_1 D_2 = 0 \quad ,$$

or:

$$i \frac{S_1}{\rho c} \sin \frac{\omega l_1}{c} \cdot i \frac{\rho c}{S_2} \sin \frac{\omega l_2}{c} + \cos \frac{\omega l_1}{c} \cos \frac{\omega l_2}{c} = 0$$

$$\cos \frac{\omega l_1}{c} \cos \frac{\omega l_2}{c} - \frac{S_1}{S_2} \sin \frac{\omega l_1}{c} \sin \frac{\omega l_2}{c} = 0$$

Introducing the parameters:

$$l = \text{total length} = l_1 + l_2 \quad ,$$

$$k = \text{ratio of the cross areas} = \frac{S_2}{S_1} \quad ,$$

$$\Delta = \text{excentricity} = \frac{1}{2} |l_1 - l_2| \quad (\text{ see fig. 3 } ) \quad \text{and}$$

$$\beta = \text{relative excentricity} = \frac{\Delta}{\frac{1}{2} l}$$

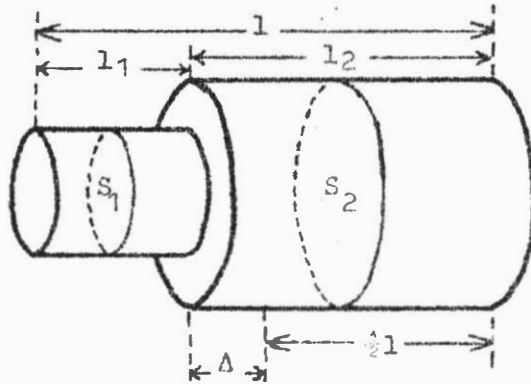
this equation can be reduced as follows:

$$\frac{1}{2} \left[ \cos \frac{\omega l}{c} + \cos \frac{\omega(l_1 - l_2)}{c} \right] + \frac{S_1}{2S_2} \left[ \cos \frac{\omega l}{c} - \cos \frac{\omega(l_1 - l_2)}{c} \right] = 0$$

$$\left( 1 + \frac{S_1}{S_2} \right) \cos \frac{\omega l}{c} + \left( 1 - \frac{S_1}{S_2} \right) \cos \frac{\omega(l_1 - l_2)}{c} = 0$$

$$\cos \frac{\omega l}{c} - \frac{1-k}{1+k} \cos \frac{2\omega \Delta}{c} = 0$$

$$\text{or: } \cos \frac{\omega l}{c} - \frac{1-k}{1+k} \cos \frac{\omega \beta l}{c} = 0 \quad (2)$$



$$\Delta = \frac{1}{2}l - l_1 = \frac{1}{2}(l_1 + l_2) - l_1 = \frac{1}{2}(l_2 - l_1)$$

Fig. 3

$\Delta$  has been introduced as an absolute value. Since it only appears under the cosine function, its sign is of no consequence.

The equation (2) is the well-known twin-tube equation in the form given by Mol. The twin-tube program starts from this equation.

Since the complexity of the expression D increases rapidly with the number of tubes, a slightly different approach must be chosen for the n-tube program ( see 4.2.5 ).

### 3.2. Bi-section method of Bolzano.

Suppose  $f(x)$  is a continuous and bounded function on  $(0, \infty)$ . We want to approximate the values of  $x$ , for which  $f(x) = 0$ . (Let us assume that such values exist.) Let these values be denoted as  $x_1, x_2, \dots, x_n, \dots$  successively. Suppose that we can find a certain value  $d$ , ( $d > 0$ ), such that for each pair of successive zeroes holds:  $x_n - x_{n-1} > d$ , and a value  $c$  ( $c > 0$ ), such that  $x_1 > c$ . Then we construct a series of trials, denoted as  $x = t_0, t_1, t_2, \dots, t_n, \dots$  in the following way.

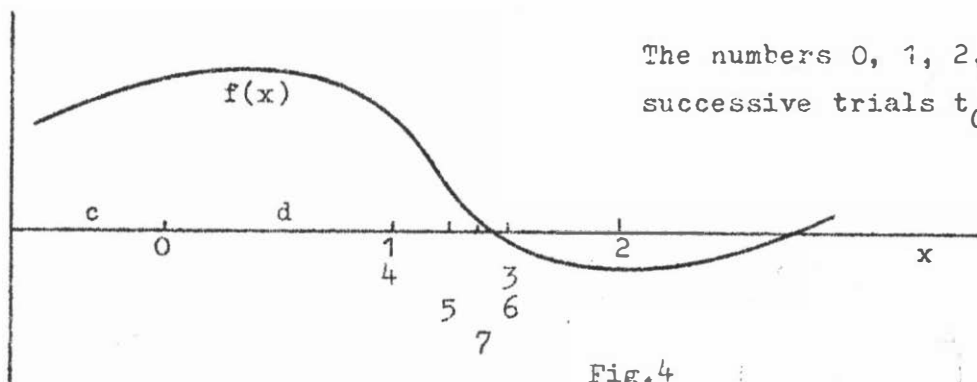


Fig.4

The first trial is:  $t_0 = c$ . We determine the sign of  $f(t_0)$ . The next trial is:  $t_1 = c + d$ , and the sign of  $f(t_1)$  is determined. If this sign is the same as the sign of  $f(t_0)$ , the next trial is:  $t_2 = c + 2d$ . In this way we continue, every time determining the sign of  $f(t_n)$ . As long as this sign is the same as that of  $f(t_0)$ , the next trial is obtained by adding  $d$  to the preceding. We assume that  $f(t_n) \neq 0$  for each  $n$ . (If  $f(t_n) = 0$  for a certain  $n$ , the zero is found, and the process is stopped.)

We continue, until we have got a trial  $t_k = c + kd$ , for which the sign of  $f(t_k)$  is opposite to the sign of  $f(t_0)$ . Then the zero  $x_1$  must be between the last two trials,  $t_{k-1}$  and  $t_k$ . We now "go backward" in steps of  $\frac{1}{2}d$  (that means:  $t_{k+1} = t_k - \frac{1}{2}d$ ;  $t_{k+2} = t_k - d$ ), again determining the sign of each  $t_n$ , until the first trial  $t_{k+i}$  for which the sign of  $f(t_{k+i})$  is opposite to the sign of  $f(t_k)$ . (Thus:  $i = 1$  or  $i = 2$ .) Then  $x_1$  must be between the last two trials, and we "go forward" in steps of  $\frac{1}{2}d$ . This process is continued until  $x_1$  is approximated sufficiently accurately.

To approximate the value of  $x_2$ , we repeat this process: we start from the approximated value of  $x_1$  and take as the first trial  $x_1 + d$ , and so on. The decision "go forward" or "go backward" must now depend on signs opposite to those, determining this decision when approximating  $x_1$ .



It is clear that the error in the approximated value of  $x_2$  is independent of that of  $x_1$ .

The iteration method here described is known as the bi-section method of Bolzano. It is well suited to high speed computers.

#### 4. Flow-chart narratives.

Both programs are self-instructing. The instructions are printed on the console printer. The keyboard is used for the input of the parameters, the punching of data decks thus being avoided.

##### 4.1. Twin-tube program.

Appendix III is a listing of the twin-tube program. Appendix I consists of:

- (1) a flow-chart of the twin-tube program,
- (2) a separate flow-chart of the calculations carried out in the twin-tube program ("CALCULATE" in flow-chart (1)).

Observing the following remarks, the course of the program can easily be read from these appendices.

4.1.1.  $c$  is defined as 35000 cm/sec, a normal value for the warm air in the vocal tract. By means of data entry switch 14 this parameter can be changed (statements 130 ff. ). In statement 145 a test is built in for extreme values of  $c$ .

4.1.2: If data switch 15 is on, the program stops.

4.1.3. Every time when reading parameter values, the program tests the field. This is realised by reading all the places out of field; if a value  $\neq 0$  is encountered, an error message is produced.

4.1.4. The counter INT causes the instruction in statement 255 to be printed once only, namely after the first run of calculations.

4.1.5. Three tests for the values of the twin-tube parameters are built in (statements 195, 205, 215.) . In the case of extreme values, the program gives error messages. The tests are the following:  
(a)  $l$  must be between 10 and 25 cm. This is only because of the practical object of the program: calculating models of the vocal

tract. Technically the program could go beyond these limits. Difficulties only arise at very great values for  $l$ , for example: a model having  $k = 8$  and  $\beta = 0$ , would produce, at an  $l$ -value of more than 1 meter, frequencies of the first and second formant so close to each other, that they would come within one single approximation step (see 3.2. and 4.1.7.).

(b)  $k$  must be between 0.1 and 10. This limitation is for mathematical reasons.

Writing the twin-tube equation (3.1.,(2)) as:

$$\cos \frac{\omega l}{c} = \frac{1-k}{1+k} \cos \frac{\omega \beta l}{c} ,$$

the solutions can be found as the intersection points of two cosine functions, one having maximal and minimal values of  $+1$  and  $-1$ , the other of  $\frac{1-k}{1+k}$  and  $-\frac{1-k}{1+k}$ . Both for great and small values of  $k$ , the value of  $\frac{1-k}{1+k}$  is close to 1.

In this case, in the neighbourhood of those values for  $\omega$  for which both functions are about maximum ( or minimum ) , there are two intersection points close to each other (see fig.5). It now may happen that these points come within one approximation step, which means that two formant frequencies may be missed.

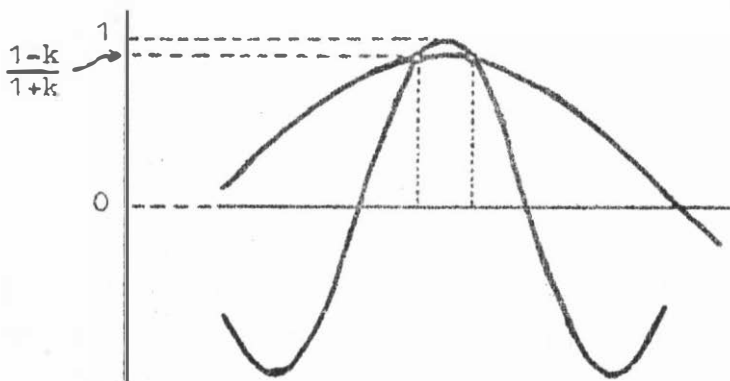


Fig.5

(c)  $\beta$  must be between  $-1$  and  $+1$ . By definition,  $\beta$  has no physical meaning for other values.

4.1.6. Statement 245 + 1 tests for the sign of the expression  $D$  (3.1.,(1)), which for the twin-tube has the form of 3.1.,(2). Two parameters  $T_1$  and  $T_2$  are used, each of which is either  $+1$  or  $-1$ .

The sign of  $T_2$  changes every time that the sign of  $D$  is changed; the sign of  $T_1$  changes every time the program starts to approximate another formant frequency. This is the way in which the decision "go forward/go backward" is governed.

Since  $0.1 \leq k \leq 10$ , (see 4.1.5., (a)), it follows that:

$$0 < \frac{1-k}{1+k} < 1 ,$$

and:

$$\cos \frac{\omega l}{c} - \frac{1-k}{1+k} \cos \frac{\omega \beta l}{c} > 0 \text{ for small values of } \omega .$$

The first trial  $t_0$  ( see 3.2.), which only served to determine the sign of the expression  $D$  for small values of  $\omega$  , can be omitted.

Both  $T_1$  and  $T_2$  are first defined as  $-1$  .

4.1.7. The value of  $F$  ( trial frequency ) is first defined as zero, and  $DF$  (increment of  $F$  ) as 32 Hz. Therefore the trials  $t_0, t_1, t_2, \dots$  are: 32, 64, 96, ....Hz, until the sign of  $D$  changes. In other words, our assumption is that the difference between two successive formant frequencies is more than 32 Hz, and the first formant frequency is more than 32 Hz.

4.1.8. In statement 235 the step length is divided by 2, and 235 + 1 tests for the step length: if this is less than  $\frac{1}{2}$  Hz, the process is stopped. Statement 250 represents a rounding-off procedure:  $\frac{1}{2}$  Hz is added to the last trial, and the figures to the right of the decimal point are deleted. This deletion is effected by the FORMAT-statement; this is not mentioned in the flow-chart. In this way we round off to the nearest whole number of Hz. If the fractional part of the last trial is exactly .5, rounding off occurs to the next greater whole number of Hz.

#### 4.2. n-tube program.

Appendix IV is a listing of the n-tube program. Appendix II contains the flow-chart, and, just as in the case of the twin-tube program, a separate flow-chart for the calculations. The following remarks refer to these appendices.

4.2.1. In three places the flow-chart has the words: WRITE INSTRUCTION, followed by a number in brackets. These numbers refer to the sections of Appendix VI where the respective instructions are shown.

4.2.2. There are two input modes:

mode 1: all tubes have the same length,

mode 2: there are tubes which have different lengths.

4.2.3. The following table gives a survey of the parameters to be entered through the keyboard and of the data entry switches by means of which the parameter values can be changed.

<u>Name_of_parameter</u>	<u>meaning</u>	<u>data_entry_switch</u>
MODE	input mode, see 4.2.2	1
NMB	number of tubes ( $\leq 20$ )	2
KTOT	number of formant frequencies to be calculated ( $\leq 4$ )	3
C	velocity of sound	4
S(I)	diameter of the Ith tube	9, to change diameters of all tubes
	{I=1, ..., NMB}	8, to change diameter of one tube only

In the case of mode 1:

LN	length of each tube	5
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In the case of mode 2:

LNGTH(I)	length of the Ith tube	7, to change lengths of all tubes
	{I= 1, ..., NMB}	6, to change length of one tube only

If data switch 6 or 8 is on, the program first inquires which tube must be changed.

Data switch 15 causes the program to stop.

The course of the program when testing for the different data switches can easily be read from the flow-chart.

Contrary to the twin-tube program, no tests are built in for parameter values and for the field. The program, therefore, is supposed to work in an error-free environment. Errors in the calculated formant frequencies are data-dependent.

4.2.4. The diameters of the tubes are specified in the input. Since the calculations are in terms of cross areas, the diameters have to be converted accordingly. Only the ratios of the cross areas are of importance, so it is sufficient to square the diameters ( statements 205-210).

4.2.5. Contrary to the twin-tube program we do not have an equation to start from. We therefore proceed as follows. The trial frequency is filled in in the four-pole coefficients of the different tubes, so that these become constants. With these constants, the matrix multiplication is carried out, which gives us the numerical value of the expression D for this trial. Depending on this value we take the next trial as described in 3.2.

In the program this is realised as follows.

After defining the trial frequency, the unit matrix is loaded in a buffer AMAT (360 ff.).

A matrix BMAT is defined as the four-pole matrix of the first tube in which the trial frequency is filled in ( depending on the mode: statements 365 ff. and 375 ff, or 380 ff.). Subsequently AMAT x BMAT is calculated (385 ff.), and this product is stored in buffer AMAT ( 385+4 ). Now BMAT is defined as the four-pole matrix of the second tube, and AMAT x BMAT is calculated again, and this product is stored buffer AMAT, and so on. When this loop is ended, the buffer AMAT contains the product of the four-pole matrices of all the tubes. Statement 410 + 1 tests for the lower-right element of this product matrix.

4.2.6. The 2x2-matrices to be multiplied contain real numbers in the principal diagonal, the other two elements being imaginary. The product of two of such matrices is of the same form again. Only the lower-right element of the product matrix is used, which is real. As a consequence of the imaginary numbers, certain terms in the product have minus signs. These are stated in the matrix multiplication in the statements 385 ff.; the factors i themselves are omitted.

4.2.7. In the lower-right element of the product matrix, the factors  $\rho c$  from the four-pole coefficients cancel each other out. This is

why they are left out in the calculations.

4.2.8.  $F$  (trial frequency) is first defined as 32 Hz, and  $DF$  (increment) as 64 Hz. The assumption, therefore, is that the first formant frequency is more than 32 Hz, and the difference between two successive formant frequencies is more than 64 Hz.

4.2.9. Two parameters  $T_1$  and  $T_2$  are used in the same way as in the twin-tube program (see 4.1.6.). For the twin-tube the sign of the expression  $D$  for small values of  $\omega$  is known beforehand. In the  $n$ -tube program this sign is determined in the first trial (32 Hz) and depending on this sign a parameter  $TT$  is set to +1 or -1 (395 ff.).

## 5. Applications.

### 5.1. Twin-tube program.

Appendix V shows an output of the twin-tube program.

5.1.1. In the first section, marked (1), the twin-tube parameters are defined on the basis of a print-plotted twin-tube model and an instruction is printed, prescribing how to enter the parameters. When the "program start"-key is pressed, three pairs of brackets are printed, in which the parameter values have to be filled in. After pressing the "end of field"-key the calculations are carried out and the formant frequencies are printed on the next line. By pressing the "program start"-key once again, new parameter values can be entered.

5.1.2. In section (2), the parameters of the model for [ə], a tube with a constant cross area, are filled in. The formant frequencies are the odd harmonics, produced by an organ pipe closed at one side and open at the other, and having a length of 17.5 cm (the average length of the male vocal tract).

5.1.3 In section (3) the parameter values of the model of Dutch [a] are filled in (see Mol, (4)).

5.1.4. In section (4) the velocity of sound is defined as 34000 cm/s (data switch 14), and the same twin-tube parameters as those in section (3) are filled in. As is to be expected, a lower value for  $c$  results in lower formant frequencies.

5.1.5. In sections (5), (6) and (7), the parameter  $l$ ,  $k$  and  $\beta$ , respectively, are out of their specified ranges ( see 4.1.5.). In each case an error message is produced and new brackets are printed. In section (8) all the parameters are within the specified ranges again.

#### 5.2. n-tube program.

The following remarks refer to the output of the n-tube program, reproduced in appendix VI.

5.2.1. In section (1) , an instruction is printed and some of the parameters are defined. After pressing the "program start"-key , brackets are printed to specify the mode, the number of tubes, the desired number of formant frequencies, and the velocity of sound.

5.2.2. In the case of mode 1, the instruction in section (3) is printed. After this, brackets are printed for the specification of the dimensions of the tubes. In section (4) the model for [  $\epsilon$  ] is calculated. Section (5) shows the output when calculating the twin-tube model for Dutch [ a ], first for  $c = 35000$  cm/s and then for  $c = 34000$  cm/s, just as is appendix V.

Whereas in the twin-tube program the ratio of the cross areas is used as a parameter, in the n-tube program it is the diameters of the tubes that have to be specified.

5.2.3. In section (6) LN is changed by means of data switch 5. The computer calculates again, the other parameters remaining unchanged. A comparison with section (5) shows that greater lengths result in lower formant frequencies ( the "law of proportional growth" , see Ungeheuer (1)).

5.2.4. If data switch 1 is on, the program branches to the beginning, immediately after the first instruction (section (7)). The mode is now defined as 2. An instruction is printed which is slightly different from that printed in the case of mode 1.

5.2.5. As can be seen in section (8) , the specification of the dimensions of the tubes takes two lines when the number of tubes is more than 10. First ten pairs of brackets are printed on one line, and after the values for the first ten tubes have been filled in and the "end of field"-key has been pressed, the remaining pairs of brackets are printed on the next line.

5.2.6. Section (9) is produced by setting data switch 8 on. Only the diameter of the 18th tube is changed; the remaining parameter values are left unchanged.

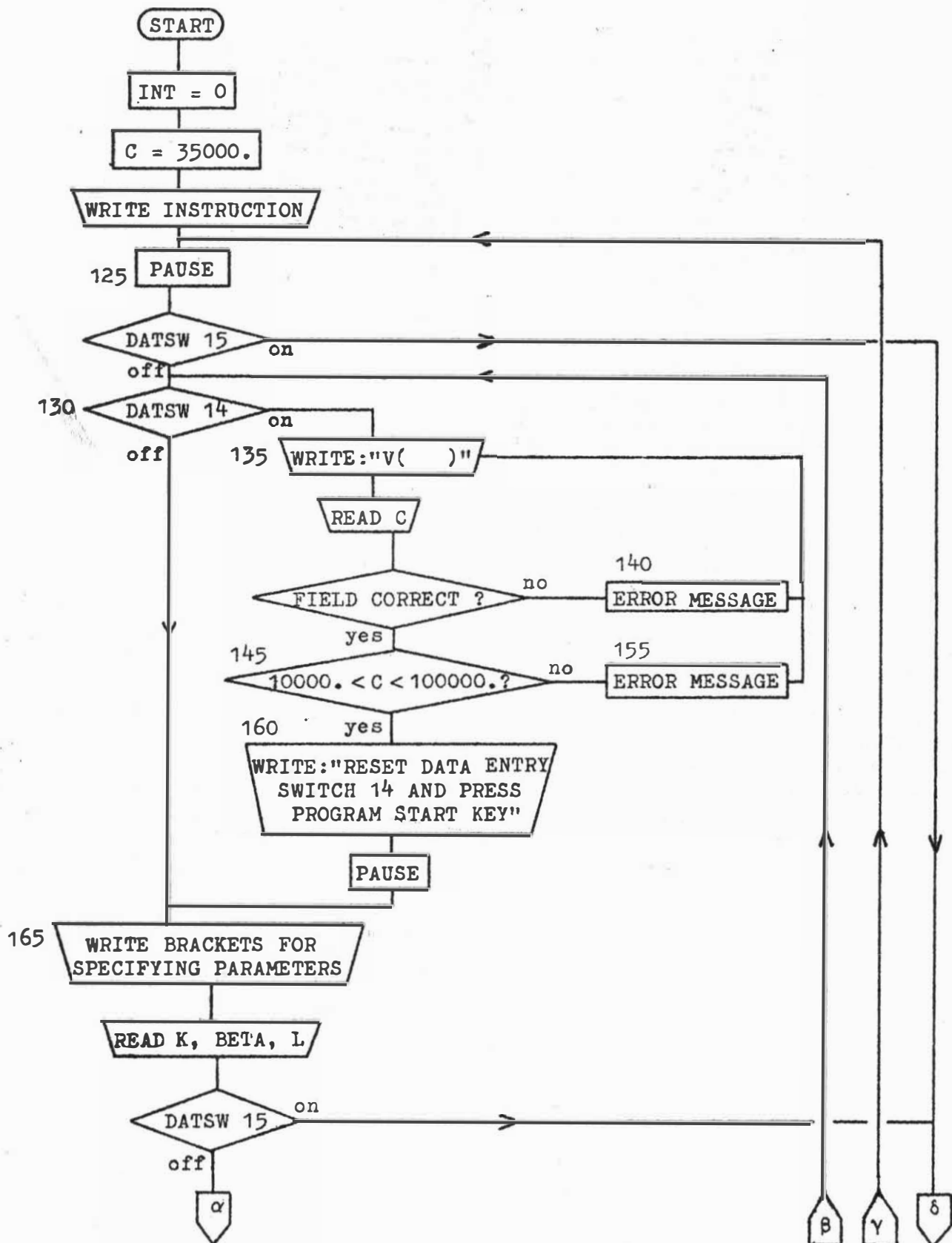
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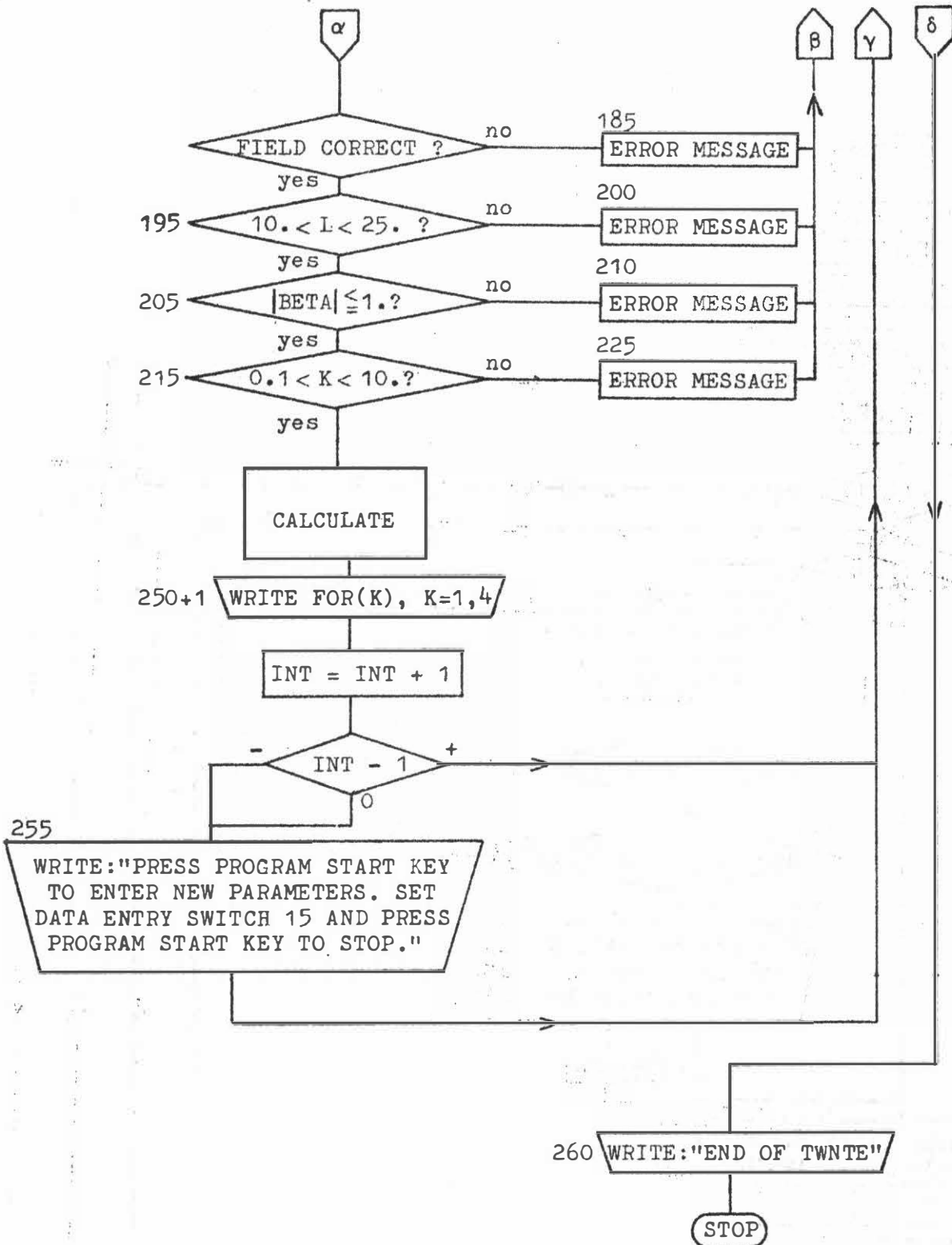
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- (1) Ungeheuer G.: Elemente einer akustischen Theorie der Vokalartikulation. (Springer 1962)
  - (2) Dunn H.K.: The calculation of vowel resonances, and an electrical vocal tract. (J.A.S.A., vol.22, p.740 ff., 1950)
  - (3) Fant G.: Acoustic theory of speech production. (Mouton 1960)
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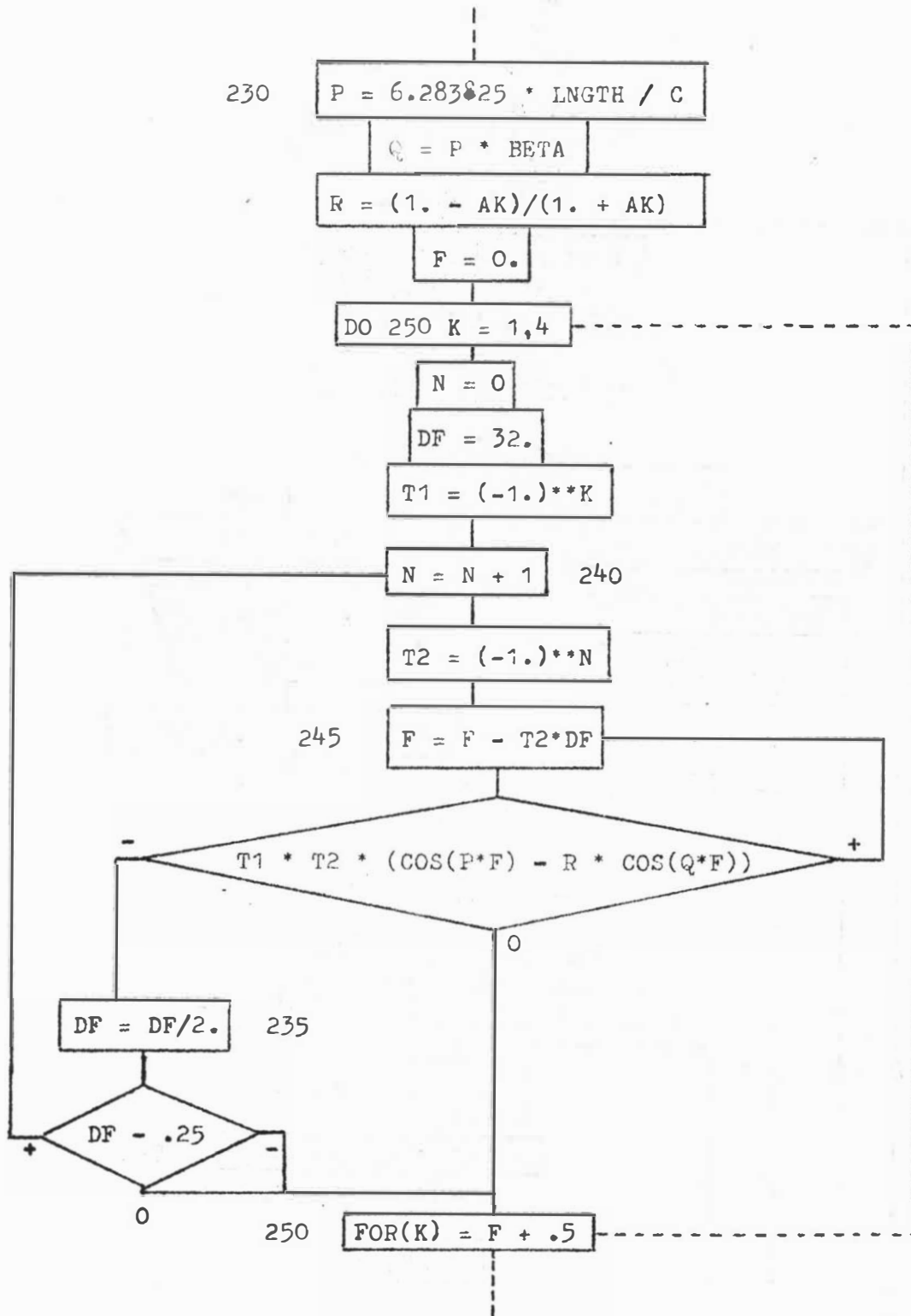
Appendix I.

(1) Flow-chart twin-tube program.



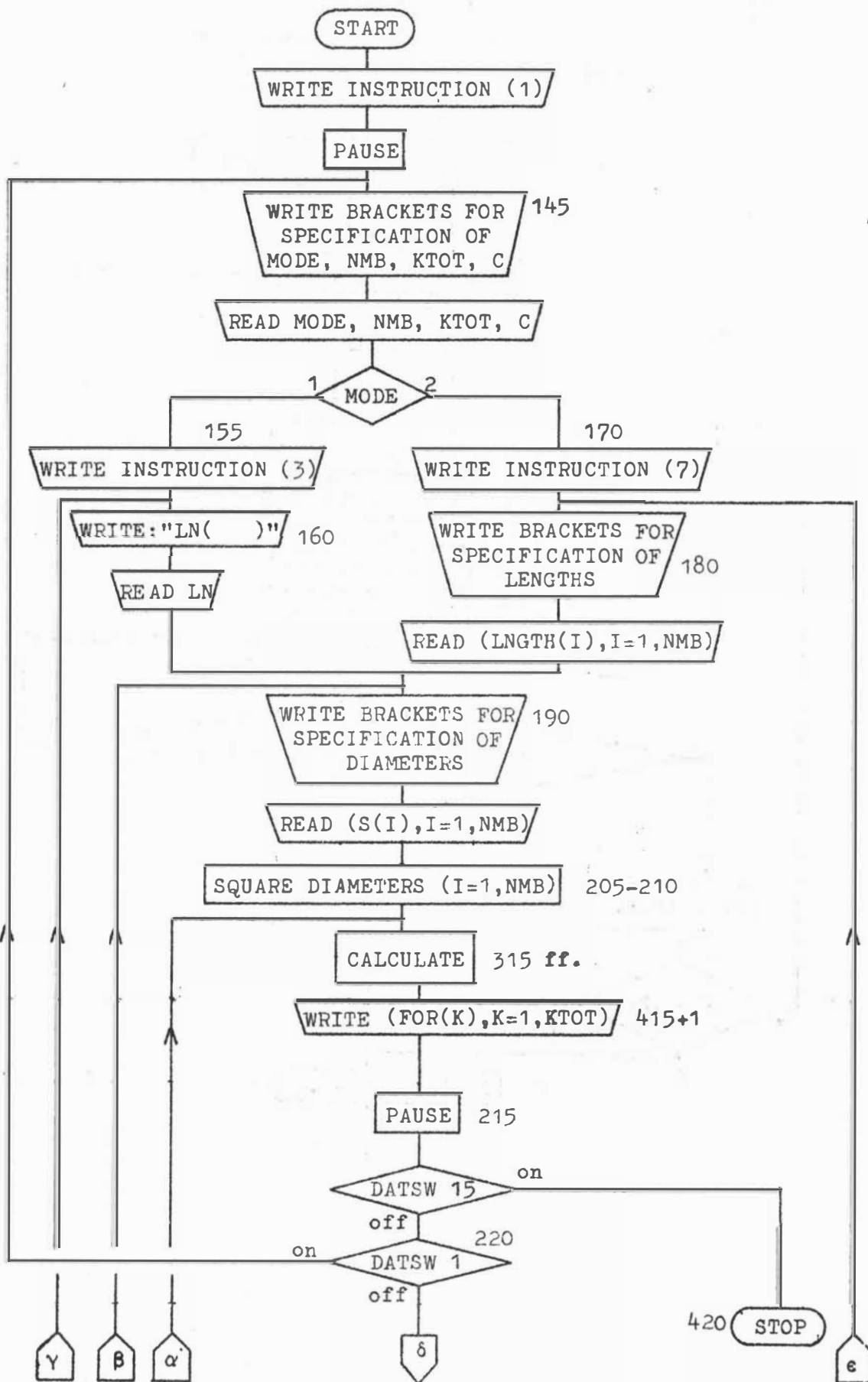


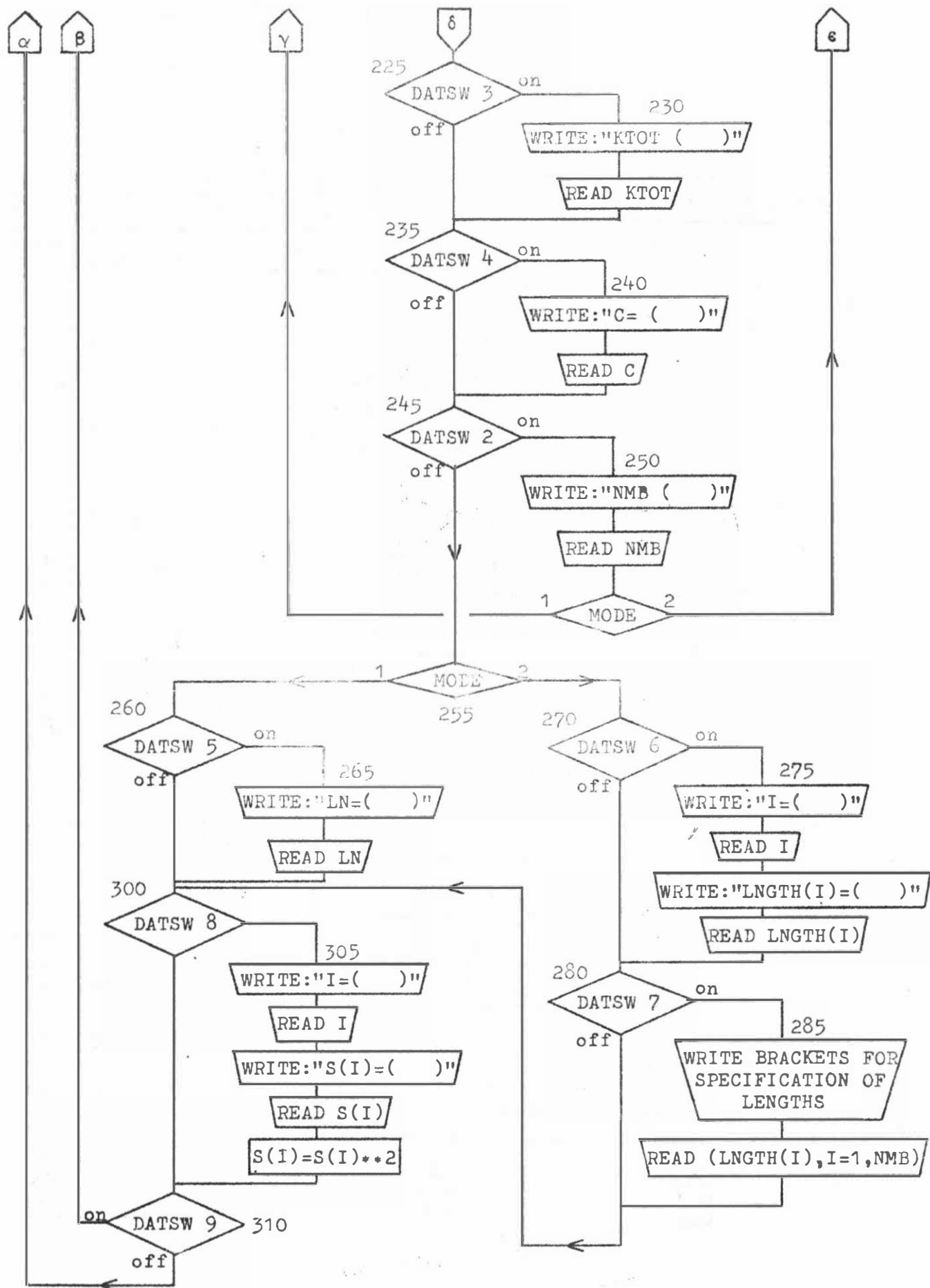
(2) Flow-chart calculations twin-tube program.



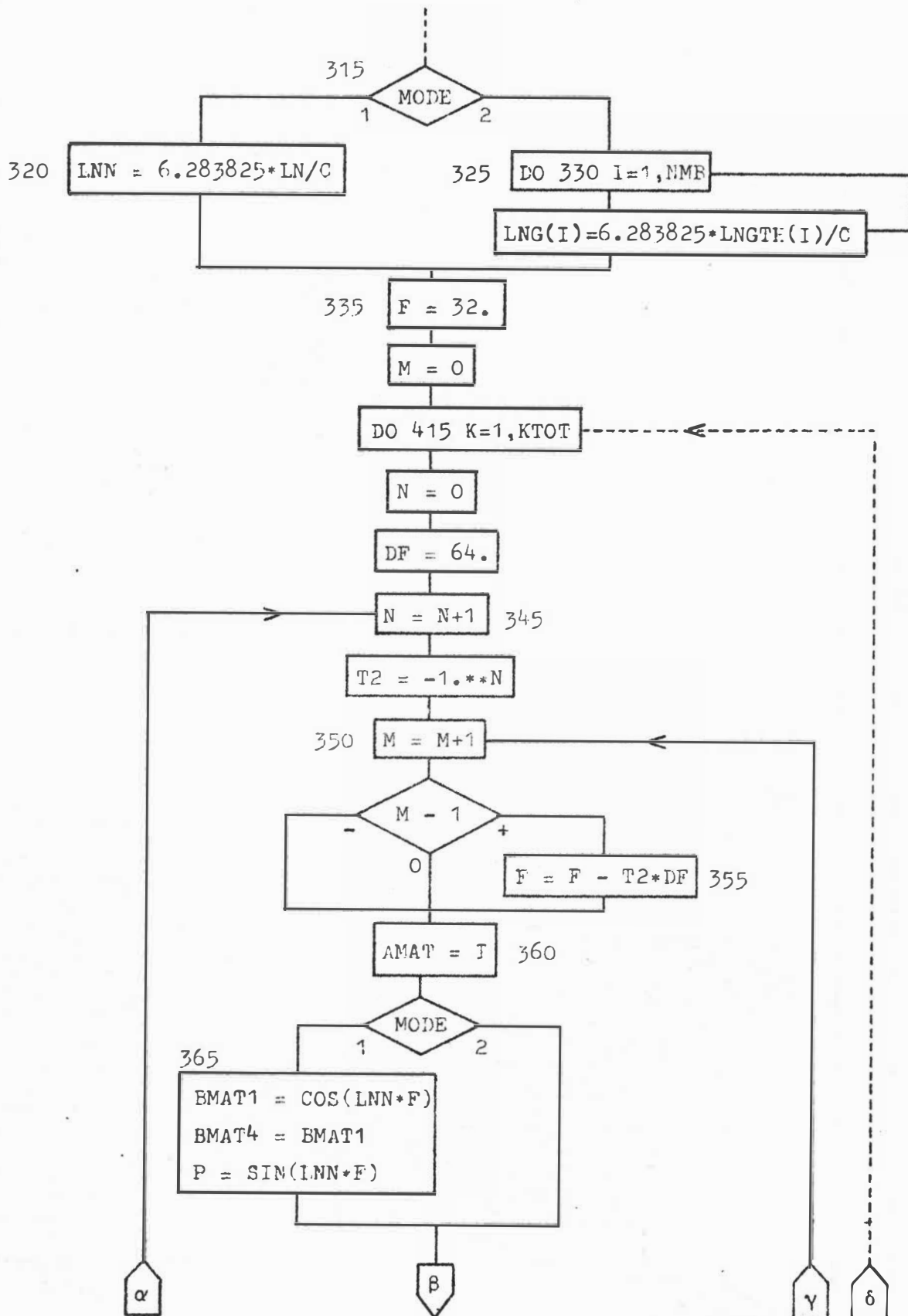
Appendix II.

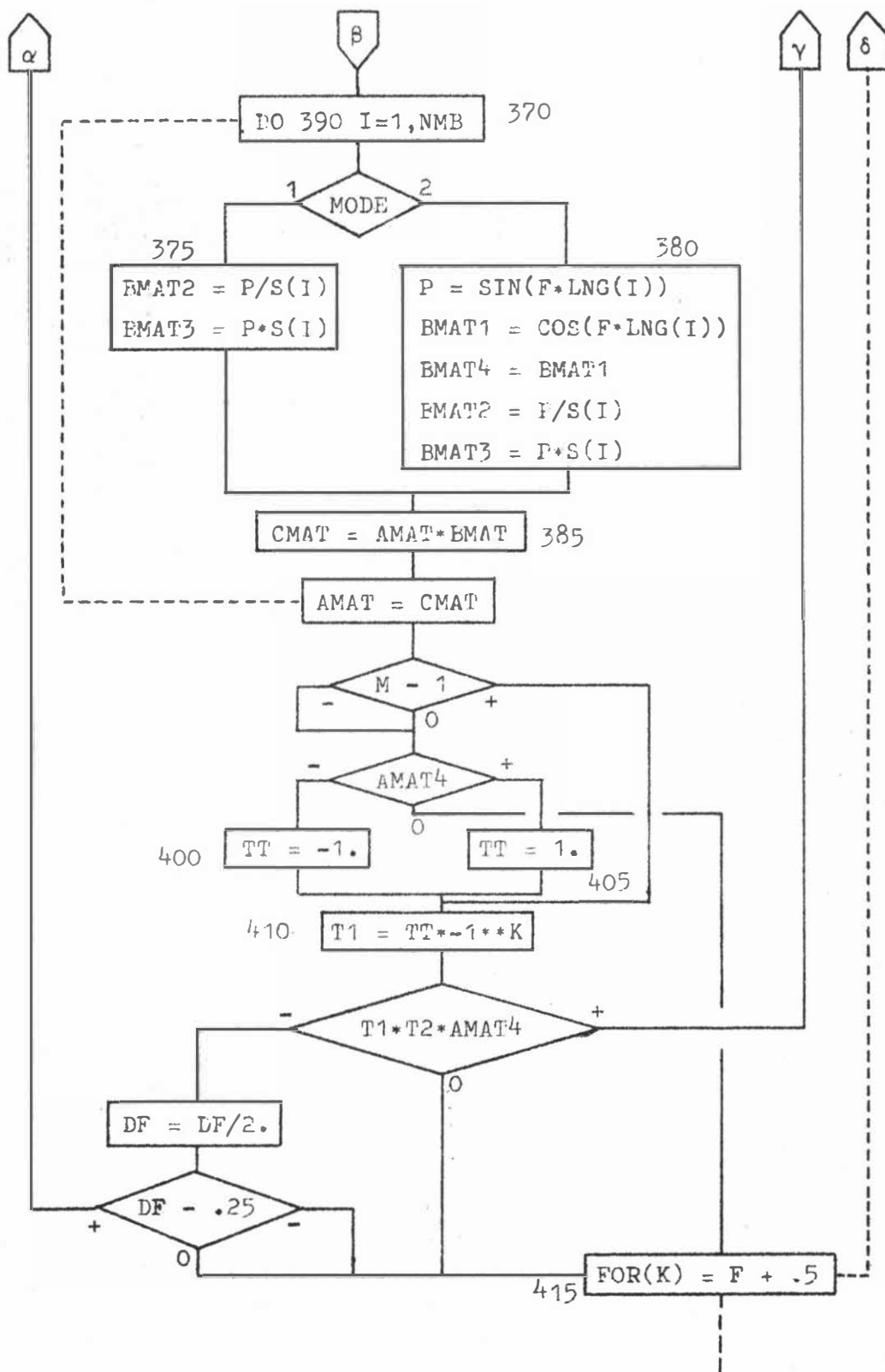
(1) Flow-chart n-tube program.





(2) Flow-chart calculations n-tube program.





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// JOB
// FOR
*LIST ALL
*IOCS(CARD,TYPEWRITER,KEYBOARD,1132PRINTER,PAPERTAPE,DISK,PLOTTER)
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```
C
C PROGRAM TWNTE
C
C THIS BASIC FORTRAN IV WRITTEN PROGRAM COMPUTES
C THE F1,F2,F3 AND F4 OF THE TWINTUBE-MODEL.
C TWNTE IS PRIMARILY WRITTEN FOR AN IBM 1130 SYSTEM,
C BUT CAN EASILY BE MODIFIED FOR EVERY COMPUTER
C WITH TYPEWRITER IN AND OUTPUT.
C
C AUTHOR J.G.BLOM.
C
C TWNTE
C REALLNGTH
C DIMENSIONA(4) ,AC(6)
5 FORMAT('PROGRAM TWNTE, I/ TWNTE COMPUTES F1,F2,F3,F4 OF THE I,
11 TWINTUBE MODEL OF THE VOCAL TRACT. I/
11 DEFINITION OF PARAMETERS. I/ )
10 FORMAT(22X, 'I, '3X, '..... I')
15 FORMAT(22X, 'I, '3X, 'I, 'I')
20 FORMAT(16X, 'I, ..... I')
25 FORMAT(6X, 'I, '15X, 'I, 'I')
30 FORMAT(6X, 'I, '5X, 'O1', 8X, 'I, '10X, 'O2')
35 FORMAT(22X, 'X D X')
40 FORMAT(16X, 'X', 5X, 'O.5L', 6X, 'X', 6X, 'O.5L', 6X, 'X' I/ I)
45 FORMAT('K=O2/O1 (RATIO OF CROSSSECTIONS) I/
11 BETA=D/O.5L (RELATIVE ECCENTRICITY) I/
11 L=LENGTH IN CM I/
11 V=35000. CM/SEC (VELOCITY OF SOUND) I)
50 FORMAT(' I/ TO CHANGE V SET DATA ENTRY SWITCH 14. I/ USE KEYBOARD TO
11 ENTER PARAMETER VALUES. I/ USE A DECIMAL POINT AND PRESS END OF FIELD
11 LD KEY. I/ IF YOU STRIKE A WRONG KEY PRESS ERASE FIELD KEY AND REENT
11 TER PARAMETERS. I/ IFIRST PRESS PROGRAM START KEY. I/ I)
55 FORMAT(8X, 'K', 15X, 'BETA', 16X, 'L' I/
13X, 'I' ) , 9X, 'I' ) , 9X, 'I' ) , 9X, 'V=', F7.0, 'CM/S')
60 FORMAT(' I/ PRESS PROGRAM START KEY TO ENTER NEW PARAMETERS. I/
11 SET DATA ENTRY SWITCH 15 AND PRESS PROGRAM START KEY TO STOP. I/ )
65 FORMAT(8X, 'V' I/ 2X, 'I' )
70 FORMAT(' ** PARAMETER OUT OF FIELD, 'I)
75 FORMAT(' ** ENTER PARAMETERS AND PRESS END OF FIELD KEY. 'I)
TWNTO010
TWNTO020
TWNTO030
TWNTO040
TWNTO050
TWNTO060
TWNTO070
TWNTO080
TWNTO090
TWNTO100
TWNTO110
TWNTO120
TWNTO130
TWNTO140
TWNTO150
TWNTO160
TWNTO170
TWNTO180
TWNTO190
TWNTO200
TWNTO210
TWNTO220
TWNTO230
TWNTO240
TWNTO250
TWNTO260
TWNTO270
TWNTO280
TWNTO290
TWNTO300
TWNTO310
TWNTO320
TWNTO330
TWNTO340
TWNTO350
TWNTO360
TWNTO370
TWNTO380
TWNTO390
```

Appendix III.  
Listing twin-tube program.



80	FORMAT('** L OUTSIDE RANGE 10,25,')	TWNT0400
85	FORMAT('** BETA OUTSIDE RANGE -1,+1,')	TWNT0410
90	FORMAT('** K OUTSIDE RANGE 0.1,10,')	TWNT0420
95	FORMAT('** V OUTSIDE RANGE 10000,100000,')	TWNT0430
100	FORMAT('RESET DATA ENTRY SWITCH 14 AND PRESS PROGRAM START KEY.')	TWNT0440
105	FORMAT('END OF TWNTE'//)	TWNT0450
110	FORMAT(3(F4.0,2F7.0))	TWNT0460
115	FORMAT(/4('F',I1,'=',F7.0,'C/S',3X)//)	TWNT0470
120	FORMAT(F4.0,F9.0,F4.0)	TWNT0480
	INT = 0	TWNT0490
	C = 35000.	TWNT0500
C	C = VELOCITY OF SOUND	TWNT0510
	WRITE(1,5)	TWNT0520
	WRITE(1,10)	TWNT0530
	WRITE(1,15)	TWNT0540
	WRITE(1,20)	TWNT0550
	WRITE(1,25)	TWNT0560
	WRITE(1,30)	TWNT0570
	WRITE(1,25)	TWNT0580
	WRITE(1,20)	TWNT0590
	WRITE(1,15)	TWNT0600
	WRITE(1,10)	TWNT0610
	WRITE(1,35)	TWNT0620
	WRITE(1,40)	TWNT0630
	WRITE(1,45)	TWNT0640
	WRITE(1,50)	TWNT0650
125	PAUSE	TWNT0660
	CALL DATSW(15,NSTOP)	TWNT0670
	GOTO(260,130),NSTOP	TWNT0680
130	CALL DATSW(14,NV)	TWNT0690
	GOTO(135,165),NV	TWNT0700
135	WRITE(1,65)	TWNT0710
	B = C.	TWNT0720
	BB = 0.	TWNT0730
	READ(6,120)B,C,BB	TWNT0740
	B = B + BB	TWNT0750
	IF (B) 140,145,140	TWNT0760
140	WRITE(1,70)	TWNT0770
	WRITE(1,75)	TWNT0780
	GOTO 135	TWNT0790
145	IF (C - 10000.) 155,150,150	TWNT0800

```

150 IF (C - 100000.) 160,160,155
155 WRITE(1,95)
    WRITE(1,75)
    GOTO 135
160 WRITE(1,100)
    PAUSE
165 WRITE(1,55)C
    DO 170 I=1,6
170 AC(I) = 0.
    READ(6,110)AC(1),AK,AC(2),AC(3),BETA,AC(4),AC(5),LNPTH,AC(6)
C    AK =RATIO OF CROSSSECTIONS
C    BETA =RELATIVE ECCENTRICITY
C    LNPTH=LENGTH OF TWIN TUBE
    CALL DATSW(15,NSTOP)
    GOTO(260,175),NSTOP
175 DO 180 I=2,6
180 AC(I) = AC(I) + AC(I)
    IF (AC(I)) 185,190,185
185 WRITE(1,70)
    WRITE(1,75)
    GOTO 130
190 IF (LNPTH - 10.) 200,195,195
195 IF (LNPTH - 25.) 205,205,200
200 WRITE(1,80)
    WRITE(1,75)
    GOTO 130
205 IF (ABS(BETA) - 1.) 215,215,210
210 WRITE(1,85)
    WRITE(1,75)
    GOTO 130
215 IF (AK - 10.) 220,220,225
220 IF (AK - .1) 225,230,230
225 WRITE(1,90)
    WRITE(1,75)
    GOTO 130
230 P = 6.283825 * LNPTH / C
    Q = 6.283825 * LNPTH / C
    R = P * BETA
    F = (1. - AK) / (1. + AK)
    F = 0.
    DO 250 K=1,4

```

```

TWNT0810
TWNT0820
TWNT0830
TWNT0840
TWNT0850
TWNT0860
TWNT0870
TWNT0880
TWNT0890
TWNT0900
TWNT0910
TWNT0920
TWNT0930
TWNT0940
TWNT0950
TWNT0960
TWNT0970
TWNT0980
TWNT0990
TWNT1000
TWNT1010
TWNT1020
TWNT1030
TWNT1040
TWNT1050
TWNT1060
TWNT1070
TWNT1080
TWNT1090
TWNT1100
TWNT1110
TWNT1120
TWNT1130
TWNT1140
TWNT1150
TWNT1160
TWNT1170
TWNT1180
TWNT1190
TWNT1200
TWNT1210

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```
N = 0
DF = 32.
T1 = ( - 1.) * * K
GOTO 240
235 DF = DF / 2.
IF (DF - .25) 250,250,240
C STOP ITERATION IF STEP SMALLER THAN .5 C/SEC.
240 N = N + 1
T2 = ( - 1.) * * N
245 F = F - T2 * DF
IF (T1 * T2 * (COS(P * F) - R * COS(Q * F))) 235,250,245
250 FOR(K) = F + .5
WRITE(1,115)(1, FOR(I), I=1,4)
INT = INT + 1
IF (INT - 1) 255,255,125
255 WRITE(1,60)
GOTO 125
260 WRITE(1,105)
CALL EXIT
END
```

```
TWNT1220
TWNT1230
TWNT1240
TWNT1250
TWNT1260
TWNT1270
TWNT1280
TWNT1290
TWNT1300
TWNT1310
TWNT1320
TWNT1330
TWNT1340
TWNT1350
TWNT1360
TWNT1370
TWNT1380
TWNT1390
TWNT1400
TWNT1410
```

```
// JOB
// FOR
*LIST ALL
*ONE WORD INTEGERS
*EXTENDED PRECISION
*IOCS(CARD,TYPEWRITER,KEYBOARD,1132PRINTER,PAPERTAPE,DISK,PLOTTER)
```

```

C
C      PROGRAM NTUBE
C
C      THIS FORTRAN IV WRITTEN PROGRAM COMPUTES F1,F2,F3 AND F4
C      OF AN N-TUBE MODEL OF THE VOCAL TRACT. NTUBE IS PRIMARILY
C      WRITTEN FOR AN IBM 1130 SYSTEM, BUT CAN EASILY BE MODIFIED
C      FOR EVERY COMPUTER WITH TYPEWRITER IN AND OUTPUT.
C
      REALLN,LNN,LENGTH(20) ,LNG(20)
      DIMENSIONS(20) ,FOR(4) ,IHAAK(8)
      5  FORMAT(//('F',I1,'=',F6.0,'HZ')//)
      10 FORMAT('PROGRAM NTUBE'//'NTUBE COMPUTES F1,F2,F3,F4 OF AN N-TUBE
      10DEL OF THE VOCAL TRACT.'//'USE INPUT MODE 1 IF ALL TUBES HAVE THE
      1  SAVE LENGTH.'//'IF THIS IS NOT THE CASE USE INPUT MODE 2.'//'NMB=NUN
      1MBER OF TUBES.'//'NMB SHOULD BE SMALLER THAN OR EQUAL TO 20.'//'KTOT
      1=NUMBER OF FORMANTS YOU WANT TO HAVE COMPUTED.'//'KTOT SHOULD BE SM
      1ALLER THAN OR EQUAL TO 4.'//'C=VELOCITY OF SOUND.'//)
      15 FORMAT('USE KEYBOARD TO ENTER THE PARAMETERS.'//'USE DECIMAL POINTS
      1  AND PRESS END OF FIELD KEY.'//'IF YOU STRIKE A WRONG KEY PRESS ERAN
      1ST FIELD KEY AND REENTER PARAMETERS.'//'TO CHANGE MODE,NMB,KTOT ORN
      1  C SET THE FOLLOWING DATA SWITCHES AND PRESS PROGRAM START KEY'//3X
      1,'MODE',6X,'1'//3X,'NMB',7X,'2'//3X,'KTOT',6X,'3'//3X,'C',9X,'4'//'IF
      1YOU CHANGE MODE,NMB KTOT AND C MUST BE REENTERED.')
      20 FORMAT('SET DATA SWITCH 15 AND PRESS PROGRAM START KEY TO STOP.'//NTUB
      1'FIRST PRLSS PROGRAM START KEY.'//)
      25 FORMAT(2X,'MODE',10X,'NMB',10X,'KTOT',10X,'C'//(' ',6X,' ')',5X,'('
      1,')',5X,'(' ',6X,' ')',4X,'(' ',10X,' ')//)
      30 FORMAT(F8.0,2F13.0,F16.0)
      35 FORMAT(//'LN=LENGTH OF EACH TUBE')
      40 FORMAT('S(I)=DIAMETER OF THE I TH TUBE'//'(I=1...NMB)'//'1=VOCAL COR
      1DS SIDE'//'NMB=MOUTH OPENING'//)
      45 FORMAT('TO CHANGE LN SET DATA SWITCH 5.')
      50 FORMAT('TO CHANGE ONE SINGLE S(I) SET DATA SWITCH 8.'//'TO CHANGE AN
      1LL THE S(I) SET DATA SWITCH 9.'//)
      55 FORMAT('LN=(',RX,')'//)
      60 FORMAT(F12.3)
      65 FORMAT(//'S(I)')

```

```

NTUB0010
NTUB0020
NTUB0030
NTUB0040
NTUB0050
NTUB0060
NTUB0070
NTUB0080
NTUB0090
NTUB0100
NTUB0110
NTUB0120
NTUB0130
NTUB0140
NTUB0150
NTUB0160
NTUB0170
NTUB0180
NTUB0190
NTUB0200
NTUB0210
NTUB0220
NTUB0230
NTUB0240
NTUB0250
NTUB0260
NTUB0270
NTUB0280
NTUB0290
NTUB0300
NTUB0310
NTUB0320
NTUB0330
NTUB0340
NTUB0350
NTUB0360
NTUB0370

```

Appendix IV.  
 Listing n-tube program.

70	FORMAT(80A1)	NTUB0380
75	FORMAT(10F8.0)	NTUB0390
80	FORMAT('LENGTH(I)=LENGTH OF THE I TH TUBE')	NTUB0400
85	FORMAT('TO CHANGE ONE SINGLE LENGTH(I) SET DATA SWITCH 6.'// 'TO CHANNTUB0410	NTUB0410
	1GE ALL THE LENGTH(I) SET DATA SWITCH 7.')	NTUB0420
90	FORMAT('LENGTH(I)')	NTUB0430
95	FORMAT('NMB ('//,6X,')//')	NTUB0440
100	FORMAT('KTOT ('//,4X,')//')	NTUB0450
105	FORMAT('C= ('//,10X,')//')	NTUB0460
110	FORMAT(F15.0)	NTUB0470
115	FORMAT('I= ('//,10X,')//')	NTUB0480
120	FORMAT('LENGTH(I)=('//,8X,')//')	NTUB0490
125	FORMAT(F20.0)	NTUB0500
130	FORMAT('S(I)=('//,8X,')//')	NTUB0510
135	FORMAT(I4,9I8)	NTUB0520
	IHAAK(1) = 19789	NTUB0530
	DO 140 I=2,7	NTUB0540
140	IHAAK(I) = 16448	NTUB0550
	IHAAK(8) = 23901	NTUB0560
	WRITE(1,10)	NTUB0570
	WRITE(1,15)	NTUB0580
	WRITE(1,20)	NTUB0590
	PAUSE	NTUB0600
	NP = 0	NTUB0610
	NPP = 0	NTUB0620
145	WRITE(1,25)	NTUB0630
	READ(6,30)AMODE,ANMB,AKTOT,C	NTUB0640
	MODE = AMODE	NTUB0650
	NMB = ANMB	NTUB0660
	KTOT = AKTOT	NTUB0670
	NM = NMB - 10	NTUB0680
	GOTO(150,165),MODE	NTUB0690
150	NP = NP + 1	NTUB0700
	IF (NP - 1) 155,155,160	NTUB0710
155	WRITE(1,35)	NTUB0720
	WRITE(1,40)	NTUB0730
	WRITE(1,45)	NTUB0740
	WRITE(1,50)	NTUB0750
160	WRITE(1,55)	NTUB0760
	READ(6,60)LN	NTUB0770
	GOTO 190	NTUB0780

165	NPP = NPP + 1	NTUB0790
	IF (NPP - 1) 170,170,175	NTUB0800
170	WRITE(1,80)	NTUB0810
	WRITE(1,40)	NTUB0820
	WRITE(1,85)	NTUB0830
	WRITE(1,50)	NTUB0840
175	WRITE(1,90)	NTUB0850
	IF (NN) 180,180,185	NTUB0860
180	WRITE(1,135)(I,I=1,NMB)	NTUB0870
	WRITE(1,70)((IHAAK(I),I=1,8),J=1,NMB)	NTUB0880
	READ(6,75)(LENGTH(I),I=1,NMB)	NTUB0890
	GOTO 190	NTUB0900
185	WRITE(1,135)(I,I=1,10)	NTUB0910
	WRITE(1,70)((IHAAK(I),I=1,8),J=1,10)	NTUB0920
	READ(6,75)(LENGTH(I),I=1,10)	NTUB0930
	WRITE(1,135)(I,I=11,NMB)	NTUB0940
	WRITE(1,70)((IHAAK(I),I=1,8),J=1,NN)	NTUB0950
	READ(6,75)(LENGTH(I),I=11,NMB)	NTUB0960
190	WRITE(1,65)	NTUB0970
	IF (NN) 195,195,200	NTUB0980
195	WRITE(1,135)(I,I=1,NMB)	NTUB0990
	WRITE(1,70)((IHAAK(I),I=1,8),J=1,NMB)	NTUB1000
	READ(6,75)(S(I),I=1,NMB)	NTUB1010
	GOTO 205	NTUB1020
200	WRITE(1,135)(I,I=1,10)	NTUB1030
	WRITE(1,70)((IHAAK(I),I=1,8),J=1,10)	NTUB1040
	READ(6,75)(S(I),I=1,10)	NTUB1050
	WRITE(1,135)(I,I=11,NMB)	NTUB1060
	WRITE(1,70)((IHAAK(I),I=1,8),J=1,NN)	NTUB1070
	READ(6,75)(S(I),I=11,NMB)	NTUB1080
205	DO 210 I=1,NMB	NTUB1090
210	S(I) = S(I) * * 2	NTUB1100
	GOTO 315	NTUB1110
215	PAUSE	NTUB1120
	CALL DATSW(15,NSTOP)	NTUB1130
	GOTO(420,220),NSTCP	NTUB1140
220	CALL DATSW(1,NMODE)	NTUB1150
	GOTO(145,225),NMODE	NTUB1160
225	CALL DATSW(3,NKTOT)	NTUB1170
	GOTO(230,235),NKTOT	NTUB1180

230	WRITE(1,100)	NTUB1190
	READ(6,60)AKTOT	NTUB1200
	KTOT = AKTOT	NTUB1210
235	CALL DATSW(4,NC)	NTUB1220
	GOTO(240,245),NC	NTUB1230
240	WRITE(1,105)	NTUB1240
	READ(6,110)C	NTUB1250
245	CALL DATSW(2,NMNB)	NTUB1260
	GOTO(250,255),NMNB	NTUB1270
250	WRITE(1,95)	NTUB1280
	READ(6,60)ANMB	NTUB1290
	NMB = ANMB	NTUB1300
	NN = NMB - 10	NTUB1310
	GOTO(160,175),MODE	NTUB1320
255	GOTO(260,270),MODE	NTUB1330
260	CALL DATSW(5,NLN)	NTUB1340
	GOTO(265,300),NLN	NTUB1350
265	WRITE(1,55)	NTUB1360
	READ(6,60)LN	NTUB1370
	GOTO 300	NTUB1380
270	CALL DATSW(6,NL)	NTUB1390
	GOTO(275,280),NL	NTUB1400
275	WRITE(1,115)	NTUB1410
	READ(6,60)AI	NTUB1420
	I = AI	NTUB1430
	WRITE(1,120)	NTUB1440
	READ(6,125)LENGTH(I)	NTUB1450
280	CALL DATSW(7,NL)	NTUB1460
	GOTO(285,300),NL	NTUB1470
285	WRITE(1,90)	NTUB1480
	IF (NN) 290,290,295	NTUB1490
290	WRITE(1,135)(I,I=1,NMB)	NTUB1500
	WRITE(1,70)((I,HAAK(I),I=1,8),J=1,NMB)	NTUB1510
	READ(6,75)(LENGTH(I),I=1,NMB)	NTUB1520
	GOTO 300	NTUB1530
295	WRITE(1,135)(I,I=1,10)	NTUB1540
	WRITE(1,70)((I,HAAK(I),I=1,8),J=1,10)	NTUB1550
	READ(6,75)(LENGTH(I),I=1,10)	NTUB1560
	WRITE(1,135)(I,I=11,NMB)	NTUB1570
	WRITE(1,70)((I,HAAK(I),I=1,8),J=1,NN)	NTUB1580

```

      READ(6,75)(LENGTH(I),I=11,NMB)
300 CALL DATSW(8,NS)
      GOTO(305,310),NS
305 WRITE(1,115)
      READ(6,60)AI
      I = AI
      WRITE(1,130)
      READ(6,110)S(I)
      S(I) = S(I) * * 2
310 CALL DATSW(9,NS)
      GOTO(190,315),NS
315 GOTO(320,225),MODE
320 LNN = 6.283825 * LN / C
      GOTO 335
325 DO 330 I=1,NMB
330 LNG(I) = 6.283825 * LENGTH(I) / C
335 F = 32.
      M = 0
      DO 415 K=1,KTOT
      N = 0
      DF = 64.
      GOTO 345
340 DF = DF / 2.
      IF (DF - .25) 415,415,345
345 N = N + 1
      T2 = ( - 1.) * * N
350 M = M + 1
      IF (M - 1) 360,360,355
355 F = F - T2 * DF
360 AMAT1 = 1.
      AMAT2 = 0.
      AMAT3 = 0.
      AMAT4 = 1.
      GOTO(365,370),MODE
365 BMAT1 = COS(LNN * F)
      BMAT4 = BYAT1
      P = SIN(LNN * F)
370 DO 390 I=1,NMB
      GOTO(375,380),MODE
375 BMAT2 = P / S(I)
      BYAT3 = P * S(I)

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```

NTUB1590
NTUB1600
NTUB1610
NTUB1620
NTUB1630
NTUB1640
NTUB1650
NTUB1660
NTUB1670
NTUB1680
NTUB1690
NTUB1700
NTUB1710
NTUB1720
NTUB1730
NTUB1740
NTUB1750
NTUB1760
NTUB1770
NTUB1780
NTUB1790
NTUB1800
NTUB1810
NTUB1820
NTUB1830
NTUB1840
NTUB1850
NTUB1860
NTUB1870
NTUB1880
NTUB1890
NTUB1900
NTUB1910
NTUB1920
NTUB1930
NTUB1940
NTUB1950
NTUB1960
NTUB1970
NTUB1980
NTUB1990

```



```

GOTO 385
380 P = SIN(F * LNG(I))
    BMAT1 = COS(F * LNG(I))
    BMAT4 = BMAT1
    BMAT2 = P / S(I)
    BMAT3 = P * S(I)
385 CMAT1 = AMAT1 * BMAT1 - AMAT2 * BMAT3
    CMAT2 = AMAT1 * BMAT2 + AMAT2 * BMAT4
    CMAT3 = AMAT3 * BMAT1 + AMAT4 * BMAT3
    CMAT4 = AMAT4 * BMAT4 - AMAT3 * BMAT2
    AMAT1 = CMAT1
    AMAT2 = CMAT2
    AMAT3 = CMAT3
390 AMAT4 = CMAT4
    IF (M - 1) 395,395,410
395 IF (AMAT4) 400,415,405
400 IT = - 1.
    GOTO 410
405 IT = 1.
410 T1 = IT * (- 1.) * * K
    IF (T1 * T2 * AMAT4) 340,415,350
415 FOR(K) = F + .5
    WRITE(1,5)(K, FOR(K), K=1, KTOT)
    GOTO 215
420 CALL EXIT
END

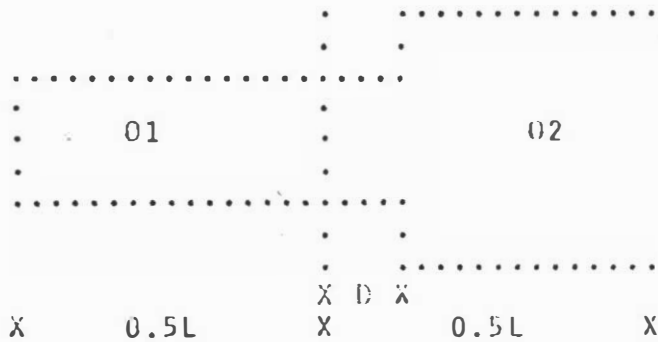
```

```

NTUB2000
NTUB2010
NTUB2020
NTUB2030
NTUB2040
NTUB2050
NTUB2060
NTUB2070
NTUB2080
NTUB2090
NTUB2100
NTUB2110
NTUB2120
NTUB2130
NTUB2140
NTUB2150
NTUB2160
NTUB2170
NTUB2180
NTUB2190
NTUB2200
NTUB2210
NTUB2220
NTUB2230
NTUB2240
NTUB2250

```

PROGRAM TWINTE,  
 TWINTE COMPUTES F1,F2,F3,F4 OF THE TWINTUBE MODEL OF THE VOCAL TRACT.  
 DEFINITION OF PARAMETERS.



K=02/01 (RATIO OF CROSSECTIONS)  
 BETA=D/0.5L (RELATIVE ECCENTRICITY)  
 L=LENGTH IN CM  
 V=35000. CM/SEC (VELOCITY OF SOUND)

TO CHANGE V SET DATA ENTRY SWITCH 14.  
 USE KEYBOARD TO ENTER PARAMETER VALUES.  
 USE A DECIMAL POINT AND PRESS END OF FIELD KEY.  
 IF YOU STRIKE A WRONG KEY PRESS ERASE FIELD KEY AND REENTER PARAMETERS.  
 FIRST PRESS PROGRAM START KEY.

( K ) ( BETA ) ( L ) V= 35000.CM/S  
 1. 17.5  
 F1= 500.C/S F2= 1500.C/S F3= 2500.C/S F4= 3500.C/S

PRESS PROGRAM START KEY TO ENTER NEW PARAMETERS.  
 SET DATA ENTRY SWITCH 15 AND PRESS PROGRAM START KEY TO STOP.

Appendix V.  
 Output twin-tube program.

(1)

(2)

( K ) ( BETA ) ( L ) V= 35000.CM/S  
 8. 17.5 (3)  
 F1= 784.C/S F2= 1217.C/S F3= 2784.C/S F4= 3217.C/S

V  
 ( 34000. )  
 RESET DATA ENTRY SWITCH 14 AND PRESS PROGRAM START KEY.

( K ) ( BETA ) ( L ) V= 34000.CM/S  
 8. 17.5 (4)  
 F1= 762.C/S F2= 1182.C/S F3= 2704.C/S F4= 3125.C/S

( K ) ( BETA ) ( L ) V= 34000.CM/S  
 5. .5 30. (5)  
 \*\* L OUTSIDE RANGE 10,25,  
 \*\* ENTER PARAMETERS AND PRESS END OF FIELD KEY.

( K ) ( BETA ) ( L ) V= 34000.CM/S  
 12. 17.5 (6)  
 \*\* K OUTSIDE RANGE 0.1,10,  
 \*\* ENTER PARAMETERS AND PRESS END OF FIELD KEY.

( K ) ( BETA ) ( L ) V= 34000.CM/S  
 8. 2. 17.5 (7)  
 \*\* BETA OUTSIDE RANGE -1,+1,  
 \*\* ENTER PARAMETERS AND PRESS END OF FIELD KEY.

( K ) ( BETA ) ( L ) V= 34000.CM/S  
 .125 .25 15. (8)  
 F1= 252.C/S F2= 1792.C/S F3= 2968.C/S F4= 3709.C/S

END OF TWNTE

PROGRAM NTUBE

NTUBE COMPUTES F1,F2,F3,F4 OF AN N-TUBE MODEL OF THE VOCAL TRACT.

USE INPUT MODE 1 IF ALL TUBES HAVE THE SAME LENGTH.

IF THIS IS NOT THE CASE USE INPUT MODE 2.

NMB=NUMBER OF TUBES.

NMB SHOULD BE SMALLER THAN OR EQUAL TO 20.

KTOT=NUMBER OF FORMANTS YOU WANT TO HAVE COMPUTED.

KTOT SHOULD BE SMALLER THAN OR EQUAL TO 4.

C=VELOCITY OF SOUND.

USE KEYBOARD TO ENTER THE PARAMETERS.

USE DECIMAL POINTS AND PRESS END OF FIELD KEY.

IF YOU STRIKE A WRONG KEY PRESS ERASE FIELD KEY AND REENTER PARAMETERS.

TO CHANGE MODE,NMB,KTOT OR C SET THE FOLLOWING DATA SWITCHES AND PRESS PROGRAM START KEY

MODE	1
NMB	2
KTOT	3
C	4

IF YOU CHANGE MODE,NMB,KTOT AND C MUST BE REENTERED.

SET DATA SWITCH 15 AND PRESS PROGRAM START KEY TO STOP.

FIRST PRESS PROGRAM START KEY.

MODE	NMB	KTOT	C
( )	( )	( )	( )
1.	1.	4.	35000.

(1)  
(2)

LN=LENGTH OF EACH TUBE  
S(I)=DIAMETER OF THE I TH TUBE  
(I=1...NMB)  
I=VOCAL CORDS SIDE  
NMB=MOUTH OPENING

(3)

TO CHANGE LN SET DATA SWITCH 5.  
TO CHANGE ONE SINGLE S(I) SET DATA SWITCH 8.  
TO CHANGE ALL THE S(I) SET DATA SWITCH 9.

LN=(            )  
          17.5

S(I)  
  1  
(            )  
  1.

(4)

F1= 500.HZ  
F2= 1500.HZ  
F3= 2500.HZ  
F4= 3500.HZ

NMB (            )  
          2.  
LN=(            )  
          6.5

S(I)  
  1            2  
(            )(            )  
  1.    2.828427

(5)

F1= 807.HZ  
F2= 1252.HZ  
F3= 2865.HZ  
F4= 3311.HZ  
C= (            )  
          34000.

F1= 784.HZ  
F2= 1216.HZ  
F3= 2783.HZ  
F4= 3216.HZ

(5)

LN=( )

8.75

F1= 761.HZ

F2= 1181.HZ

F3= 2704.HZ

F4= 3124.HZ

}  
(6)  
}

( MODE ) ( NMB ) ( KTOT ) ( C )

2. 18. 4. 35000.

LNTH(I)=LENGTH OF THE I TH TUBE  
S(I)=DIAMETER OF THE I TH TUBE

(I=1...NMB)  
I=VOCAL CORDS SIDE  
NMB=MOOUTH OPENING

TO CHANGE ONE SINGLE LNTH(I) SET DATA SWITCH 6.  
TO CHANGE ALL THE LNTH(I) SET DATA SWITCH 7.  
TO CHANGE ONE SINGLE S(I) SET DATA SWITCH 8.  
TO CHANGE ALL THE S(I) SET DATA SWITCH 9.

}  
(7)  
}

LNTH(I)  
( 1 ) ( 2 ) ( 3 ) ( 4 ) ( 5 ) ( 6 ) ( 7 ) ( 8 ) ( 9 ) ( 10 )  
( .6 ) ( .6 ) ( .6 ) ( .6 ) ( .6 ) ( .6 ) ( .6 ) ( .6 ) ( .6 ) ( .6 )

( 11 ) ( 12 ) ( 13 ) ( 14 ) ( 15 ) ( 16 ) ( 17 ) ( 18 )  
( .6 ) ( .6 ) ( .6 ) ( .6 ) ( .6 ) ( 3. ) ( 3. ) ( 3. )

}  
(8)  
|

S(1)  
 1            2            3            4            5            6            7            8            9            10  
 (            ) (            ) (            ) (            ) (            ) (            ) (            ) (            ) (            ) (            )  
   1.            1.2            1.4            1.6            1.8            2.            2.2            2.4            2.3            2.1            )

11            12            13            14            15            16            17            18  
 (            ) (            ) (            ) (            ) (            ) (            ) (            ) (            )  
   1.9            1.7            1.6            1.5            1.4            1.3            1.2            1.3

F1= 377.HZ  
 F2= 1677.HZ  
 F3= 2744.HZ  
 F4= 3482.HZ

I= (            )

S(1)=(            18.            )  
           1.1

F1= 357.HZ  
 F2= 1613.HZ  
 F3= 2735.HZ  
 F4= 3510.HZ



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